Jackson Highway Tiny Homes

Centralia, WA

Pump Study

Fuller Designs Project No. 2030 July 20, 2021 Revised: Sept. 7, 2021



Project Information

Prepared for:	Jackson Highway Tiny Homes 2945 Jackson Highway Chehalis, WA 98532
Contact:	David Cosser 282 Southwest 13 th Street Chehalis, WA 98532

Reviewing Agency

Jurisdiction:	City of Chehalis 2007 Northeast Kresky Avenue Chehalis, WA 98532
	Lewis County Water and Sewer District #4 P.O. Box 1122 Chehalis, WA 98532
Contact:	City Engineer, Trent Lougheed, (360) 748-0238 Sewer District Representative, Patrick Wiltzius, (360) 269-3657

References

Project Engineer

Prepared by: Fuller Designs, Inc. 1101 Kresky Ave Centralia, WA 98531 (360) 807-4420 Contact: Aaron Fuller, PE

"I hereby certify that this Pump Study for the Jackson Highway Tiny Homes Project has been prepared by me or under my supervision.





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Pump Study

1. Overview

This report serves as an evaluation of the Logan Hill Lift Station along Jackson Highway between Logan Hill Road and Yates Road in Chehalis, Washington. This Pump Study will determine if the existing lift station can manage the additional effluent brought about by the proposed 62-lot Jackson Highway Tiny House Development.

2. EXISTING CONDITIONS

As-built drawings provided by the City of Chehalis indicated two pumps were housed in a circular vault, and valves and pig port in a rectangular vault, Figure 2.1. Upon inspection, three vaults were present onsite, Figure 2.2.

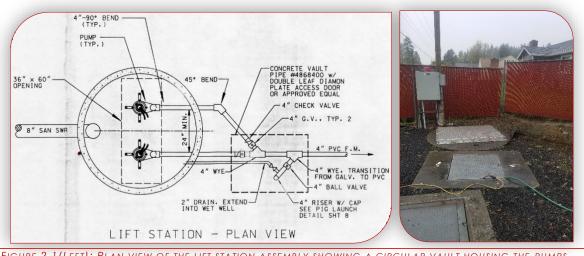


FIGURE 2.1 (LEFT): PLAN VIEW OF THE LIFT STATION ASSEMBLY SHOWING A CIRCULAR VAULT HOUSING THE PUMPS AND A RECTANGULAR VAULT HOUSING THE VALVES AND PIG PORT. FIGURE 2.2 (RIGHT): SITE PHOTO WITH THREE VAULTS PRESENT HOUSING THE PUMPS (FARTHEST), VALVES (MIDDLE) AND THE PIG PORT (PARTIAL VIEW).

Analyzing the differing layout indicated the check-valve, gate-valve, pigging port, and tee vault had been split into two vaults. Valves in middle vault with pig port and tees in the other. While different in configuration, the system operates as shown in the asbuilt plans included in <u>Appendix A</u>.

An interview with District #4 Commissioner, Patrick Wiltzius, yielded information that the system had never been expanded since the lift station's installation in 1996. Onsite pumps were identified as the Myers 4VX50M4-23 Solids Handling Wastewater Pump 5.0 with a 7" impeller (Myers Pump). The pump performance curve was provided by the manufacturer and can be found in <u>Appendix A</u> of this report. Sometime during 2018, one of the pumps was replaced along with one of the check valves and corresponding isolation valves. The other check valve was repaired at this time as well. The City of Centralia is currently in the process of repairing the impeller on the additional pump.



Attempts to find additional information was made through phone calls and emails with Lewis County, Water/Sewer District #4 and City of Chehalis. Long term energy usage or records of existing sewage flow rates could not be acquired. Maintenance logs of the station were not available. Other than an interview with Mr. Wiltzius, additional information concerning the lift station and pumps was limited and therefore, the following assumptions were made.

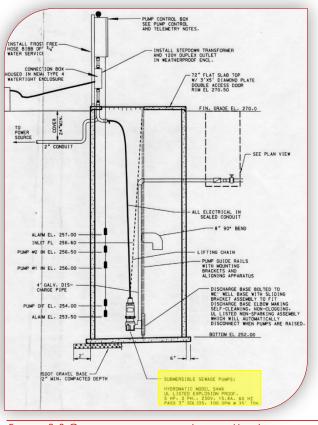


FIGURE 2.3 CROSS SECTION OF THE LOGAN HILL LIFT STATION PUMP SPECIFICATIONS HIGHLIGHTED.

Assumptions

Inflow

Information concerning the existing inflow to the lift station could not be found, however the interview with Mr. Wiltzius yielded the lift station had never been expanded. This indicated original laterals in the as-built drawings are the only service lines contributing to the lift station. A parcel map was generated, Appendix A, highlighting the 26 parcels that were serviced by the lift station in 1996. Today, the current land use of the 26 parcels includes18 residential lots, one commercial lot and seven lots that are government/ land use properties.

Average person produces between 50 to 70 gallons of wastewater per day¹. Assuming the average home serviced by the lift station is three bedrooms with two people per room, the average daily flow from one residential home can be assumed as 360gal/day. The average daily flow from the 18 residential parcels can be estimated as 6,480gal/day (4.5-GPM). This is considered a reasonable value as commonly accepted septic design regulation is consistent with 360-gal/day for a standard single-family residence (120-gal/day per bedroom).

The commercial property, Creekside Event Center,

serviced by the lift station has a seating capacity of 200-people. During an event each person is expected to use 10-gal of water. Assuming a peak event, it can be estimated 2,000-gal/day of effluent is entering the lift station from this commercial property. However, the US Department of Health suggests event centers have relatively small sewer usage during periods of inactivity.

The remaining seven government/ land use properties were considered to have no effects on the lift station as no buildings are present on these properties. Therefore, it can be concluded that the existing inflow into the pump is 8,480-gal/day (5.9-GPM).

¹ Benefield, Laura A. RESIDENTIAL FLOW RATES, 2002, pp. 1–18, RESIDENTIAL FLOW RATES.

3. EVALUATION

This report serves to evaluate if the current lift station can accommodate an additional increase in sewage brought about by the proposed Jackson Highway Tiny Home Development (Development). The Development proposes the installment of 62 residential homes. These homes are expected to be approximately 900SF and only have 1-2 bedrooms. Assuming 2 bedrooms at 120-gal/day the proposed homes are expected to produce a sewage output of 240-gal/day from each home. This is an estimated increase of 14,880-gal/day (10.3-GPM).

As stormwater should not enter the sewer lift station, effects of storm events were not considered or evaluated in this pump study. Fuller Designs' recommendations to lessen the effects of storm events on the lift station can be found in <u>Section 4</u> of this report.

Existing Peak Flow & Cycle Time

Under the existing conditions, it was determined the average per minute inflow is currently 5.9-GPM. This flow rarely happens as usage drops to minimal during the middle of the day and at

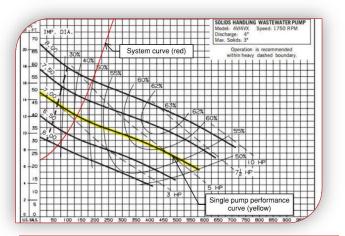


FIGURE 3.1 THE SYSTEM CURVE (RED) AND PUMP PERFORMANCE CURVE, WHEN A SINGLE PUMP IS WORKING (YELLOW). AN ENLARGEMENT OF THE GRAPH CAN BE FOUND IN APPENDIX A.

night. Peak usage is usually obtained by measuring peak discharge events and comparing these values to average rates. The assumed peaking factor for this station is 4 (Section C1-3.3.2 of the DOE Sewage Works Design – Orange Book)². It can be concluded the existing peak inflow to the system is approximately 23.6-GPM. This rate can be assumed to be sustained for one hour.

Analysis of the pumping cycle assumes a beginning point with effluent at the pump off level and beginning a peak hour. After 12.5-min, with an effluent inflow rate of 23.6-GPM, Pump One switches to the on position. Pump one begins to discharge effluent from the station at a rate of 125-GPM. This rate was determined by the approximate crossing of the system curve and the

single Myers pump curve, Figure 3.1. The volume of effluent in the lift station will decrease by 101.4-GPM when working at a rate of 125-GPM, Pump One switches to the off position after 2.9min, completing the cycle at 15.4-min. During one hour of peak flow, this results in 4 cycles in a peak hour with the pump running for approximately 11.6 minutes during that timeframe. Cycles during lower flow conditions are significantly longer with extended pump off times.

Under the current conditions, it was concluded that Pump Two only comes on as an emergency backup.

² Criteria for Sewage Works Design, Aug 2008, pp. C1-7, Fig C1-1, Dep. of Ecology.

Proposed Peak Flow & Cycle Time

The proposed development is expected to increase the total effluent into the system by an additional 10.3 GPM. The flow is expected to be a total of 16.2-GPM. Under the same peaking factor of 4, it is expected the resulting effluent during an hourly peak event will be 64.8-GPM.

Assuming the conditions remain as existing inside the lift station except for the increased effluent flow, during peak flow events it is expected Pump One will switch on after 4.53-min. Discharging at a rate of 125-GPM, the effluent is expected to discharge from the lift station at a rate of 60.2-GPM. Pump One is expected to switch off after 4.9-min of pumping. The results in a 9.4-min pump cycle. In this proposed condition peak hour scenario, the pump is expected to cycle approximately 6 times during this timeframe. Cycles during lower flow conditions are significantly longer with extended pump off times.

Similarly, to the existing conditions, in this proposed scenario, Pump Two would work as a full backup and only expected to be used in an emergency.

4. Recommendations

It is Fuller Designs' recommendation that the existing pumps may serve the proposed development without significant improvement. With increased pumping cycles, it is expected Pump maintenance intervals will also increase. As new developments are implemented and continue to tax this station, the cycles will slowly decrease and pump on time will also increase.

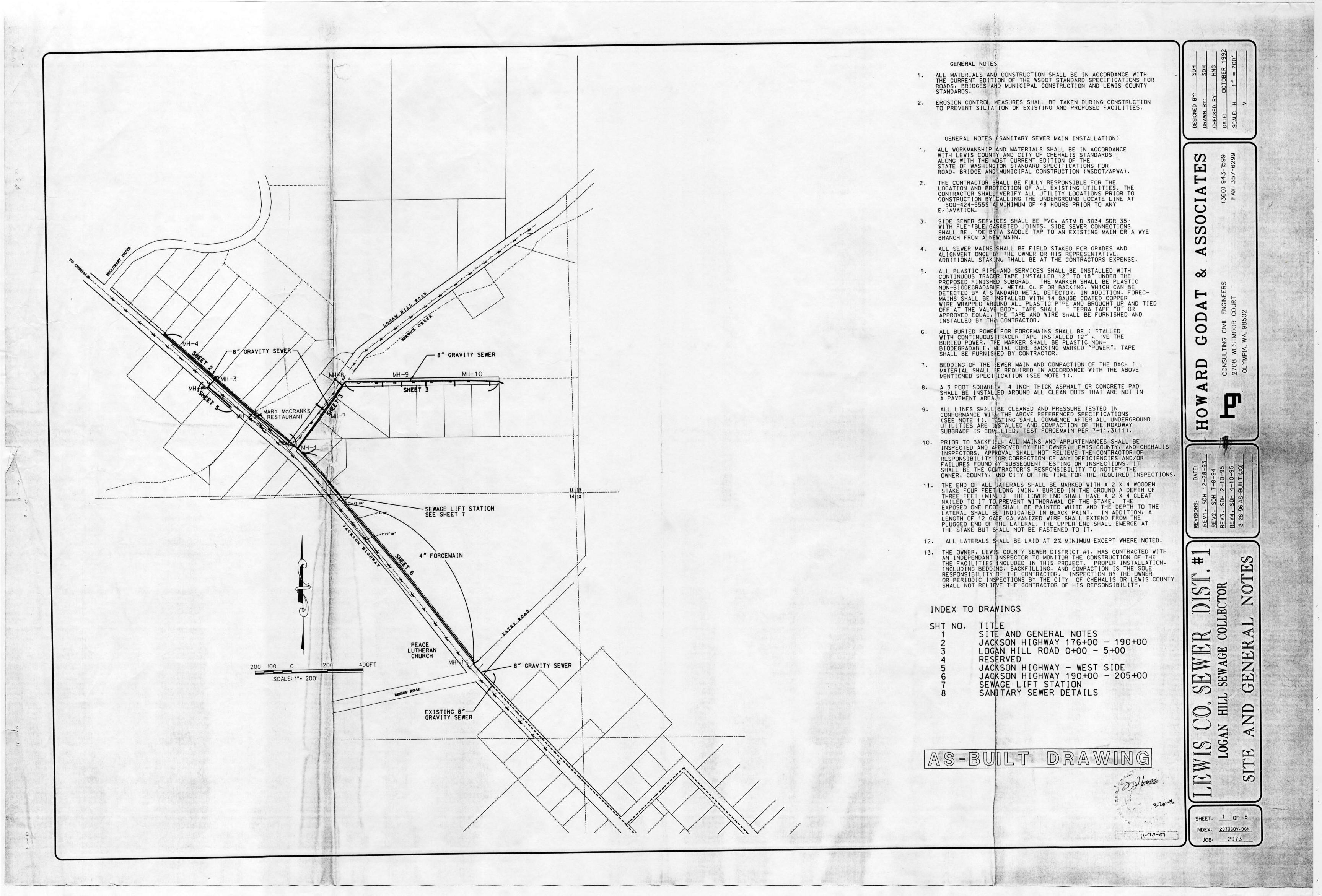
It is recommended these pumps be serviced in a standard fashion in line with manufactures recommendations, checking for wear periodically. Depending on timeframe of the last pump check, Fuller Designs recommends a check including removal, disassembly, and visually checking impeller and volute (pump housing) for wear. If significant wear is observed a rebuild or replacement may be in order. Consideration to extend the maintenance interval of these pumps may be periodically switched between Pump One and Pump Two communication and power leads. This will change the primary pump, split wear between the pumps, and extend the life of the station.

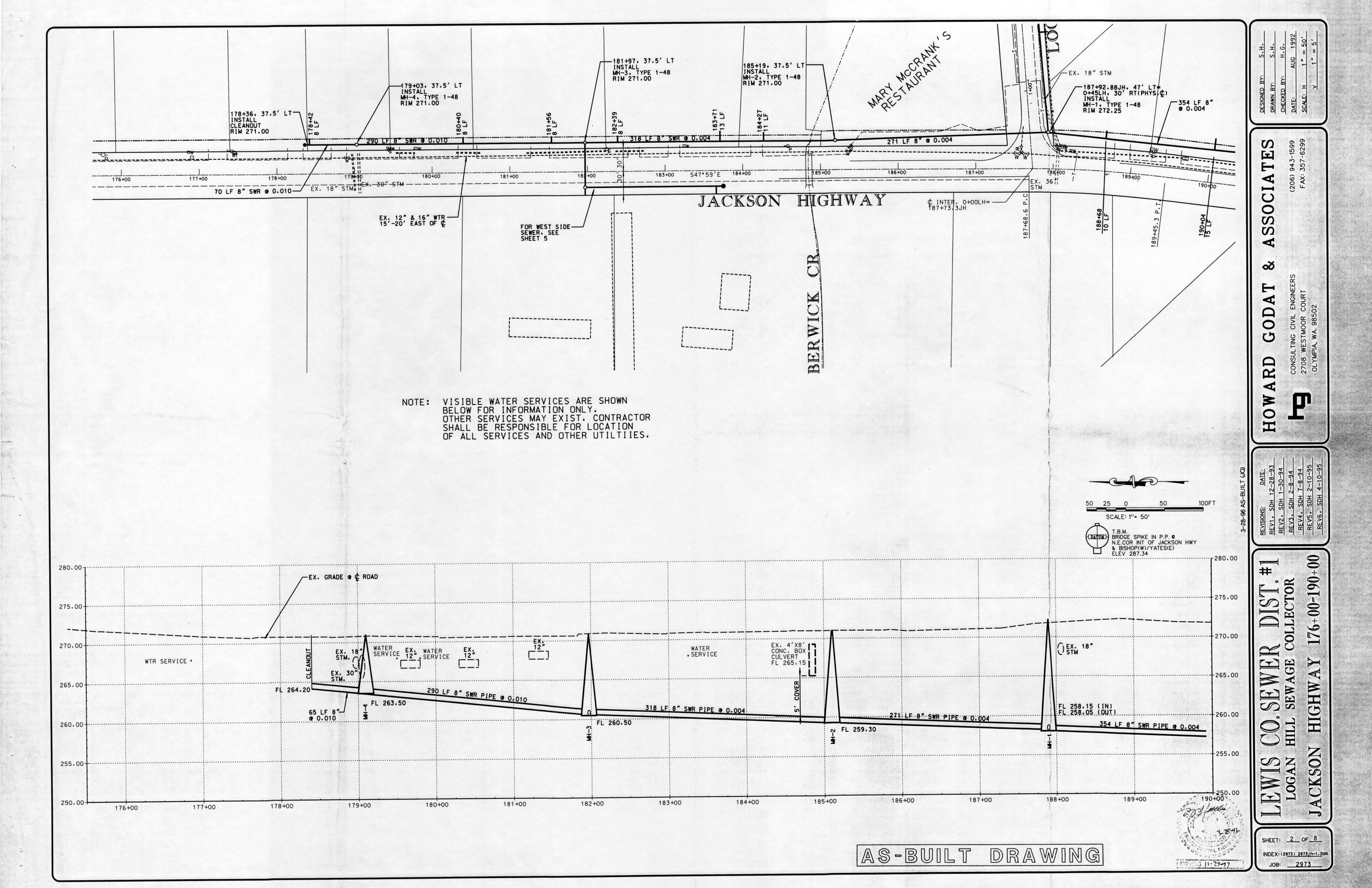
Fuller Designs also recommends the use of watertight lids and additional stormwater separation techniques. Specifically rerouting the stormwater ditch that runs through the pump station. These actions will help alleviate the effects of stormwater entering the lift station during large storm events.



APPENDIX A

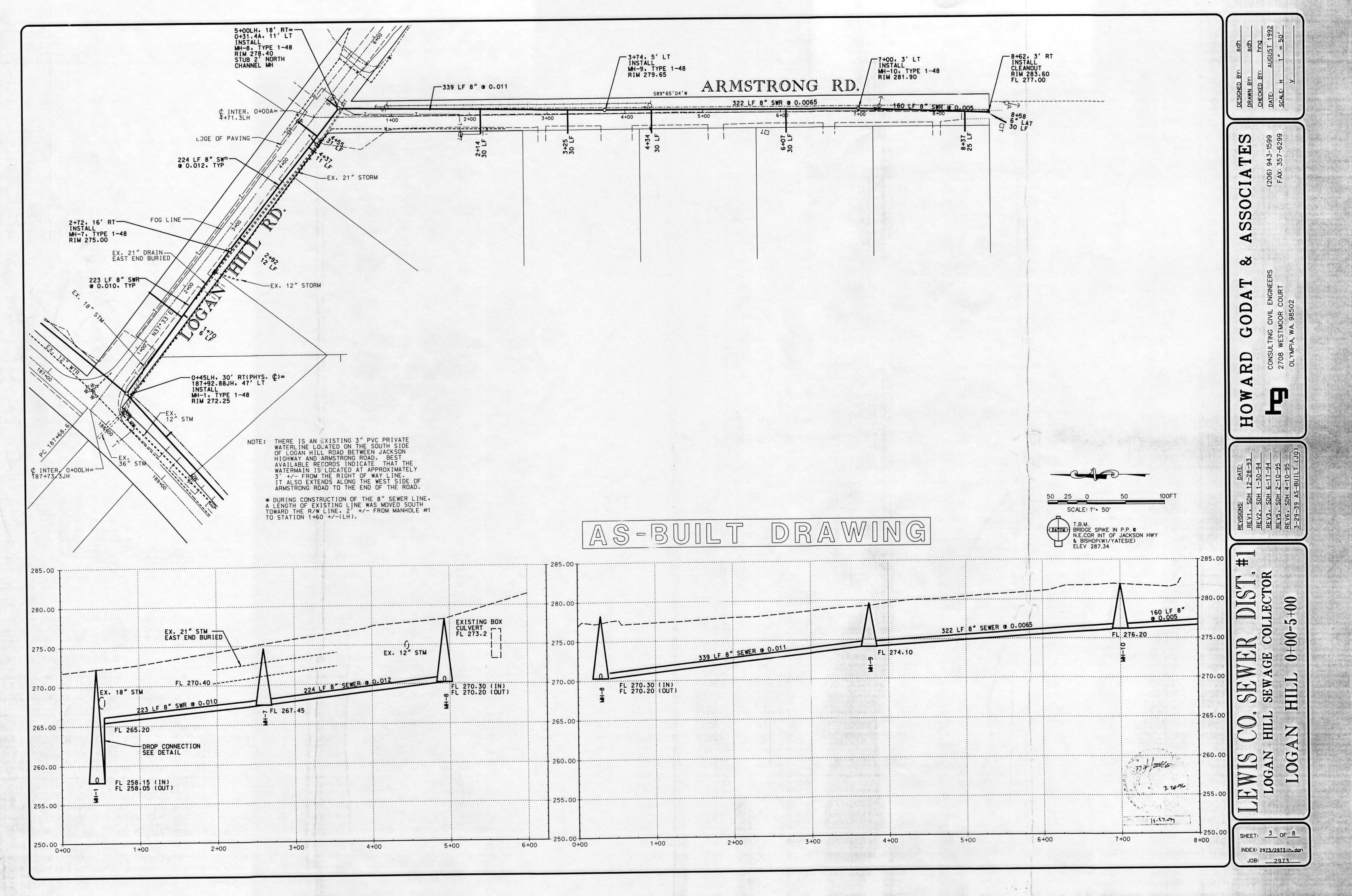






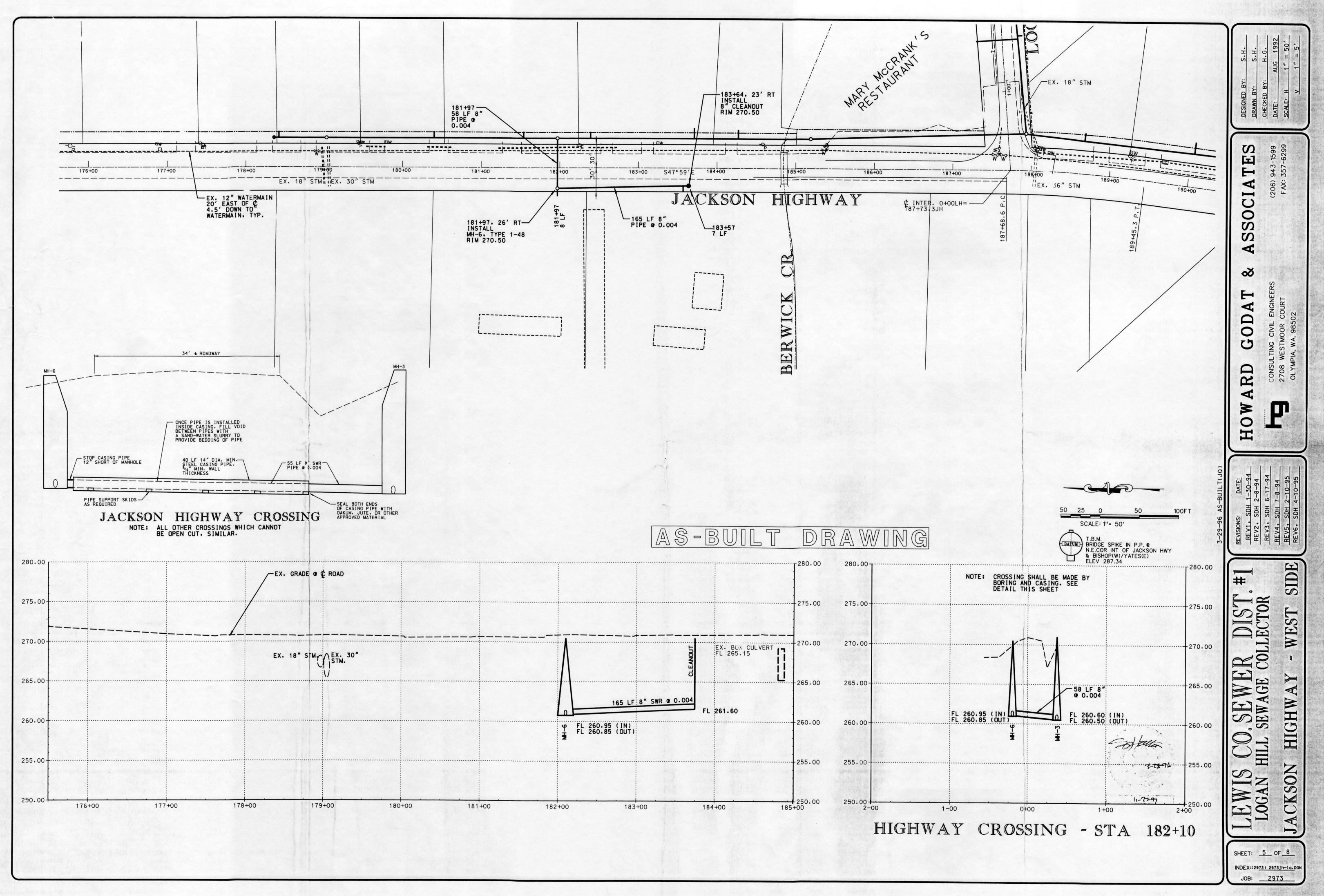
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PIPE @ O.		318 LF	8" SWR PIPE @ 0.004	5' COVER		271. LF8". SWR PIPE
	ľ J	FL 260.50			N FL 259.30	
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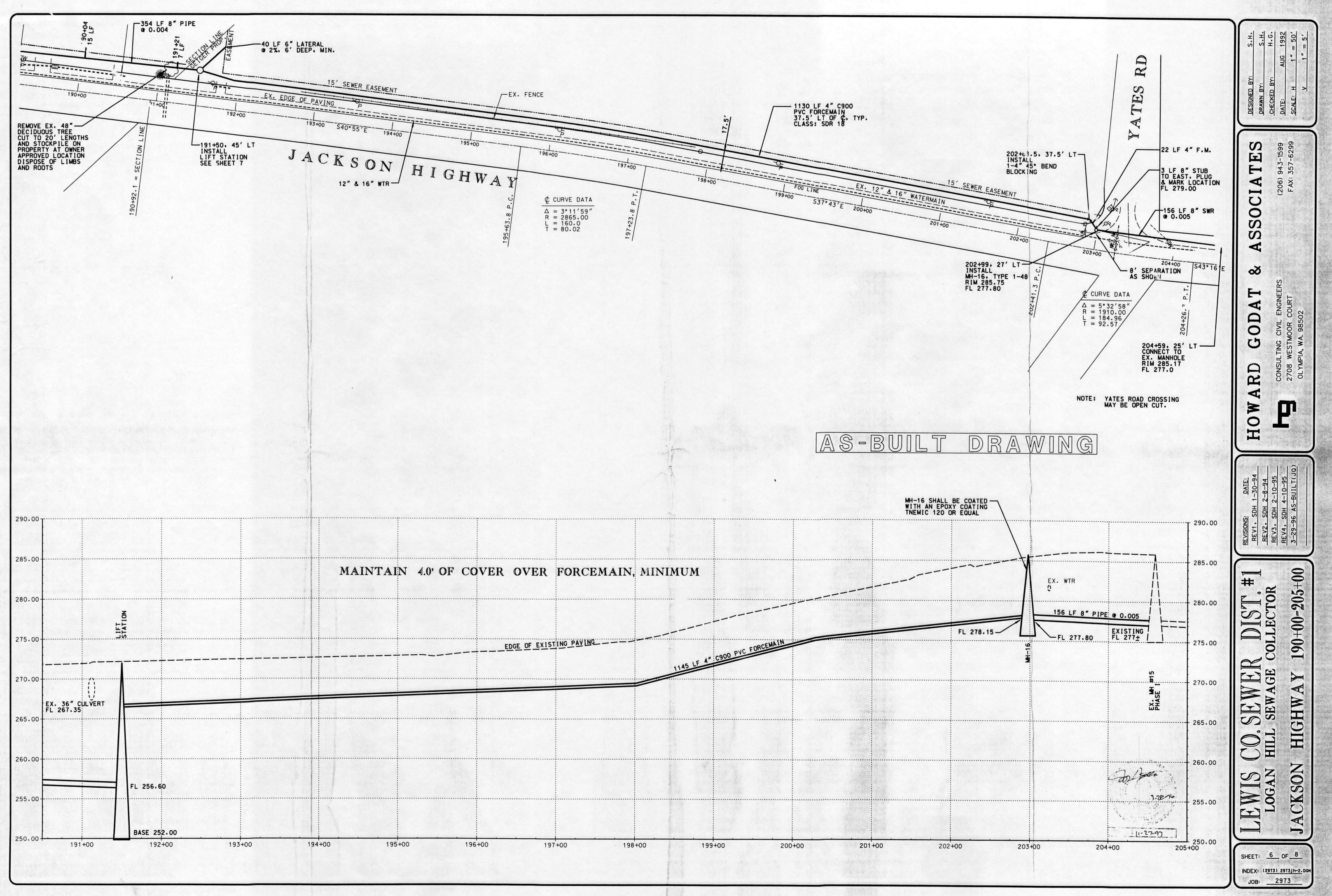
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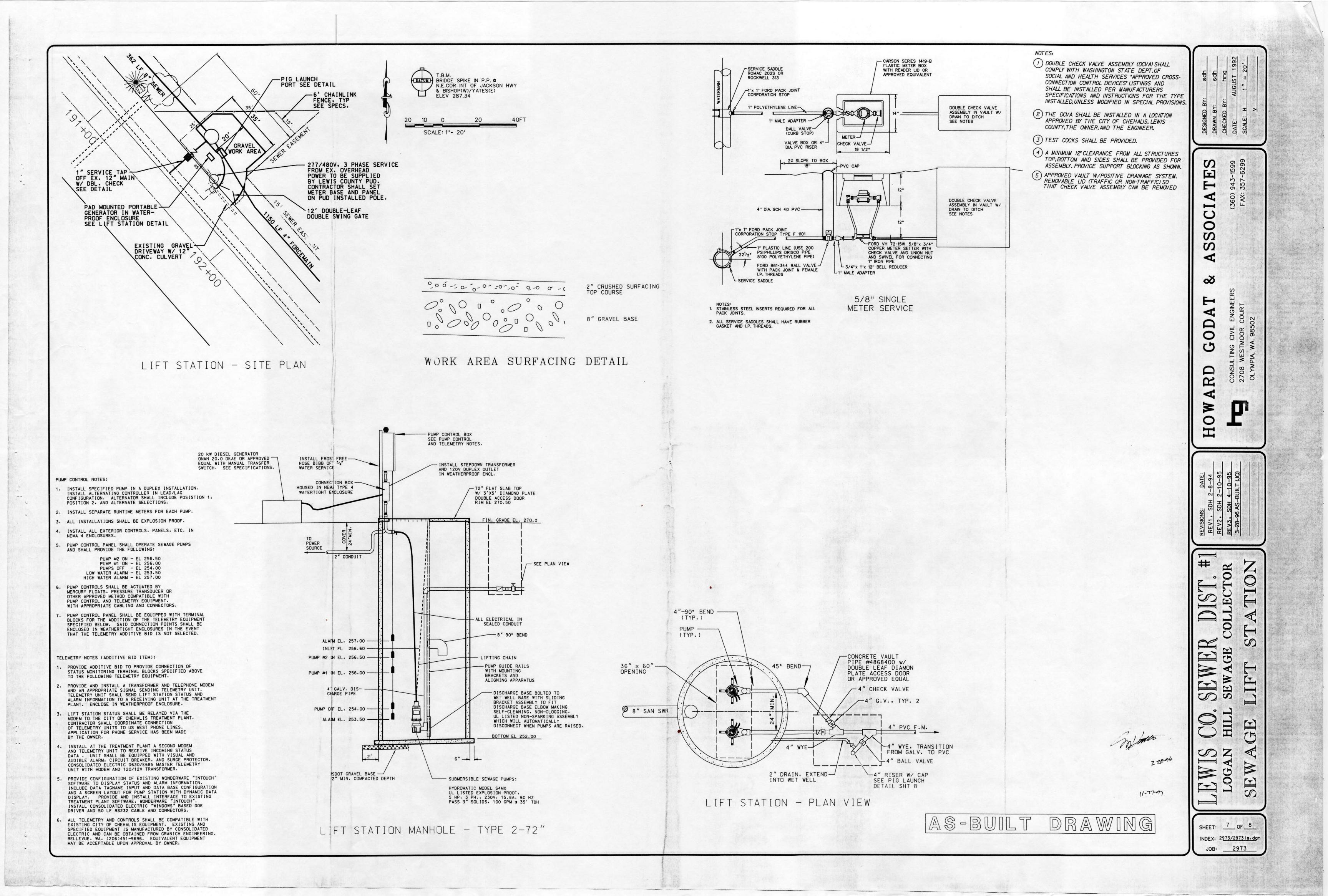


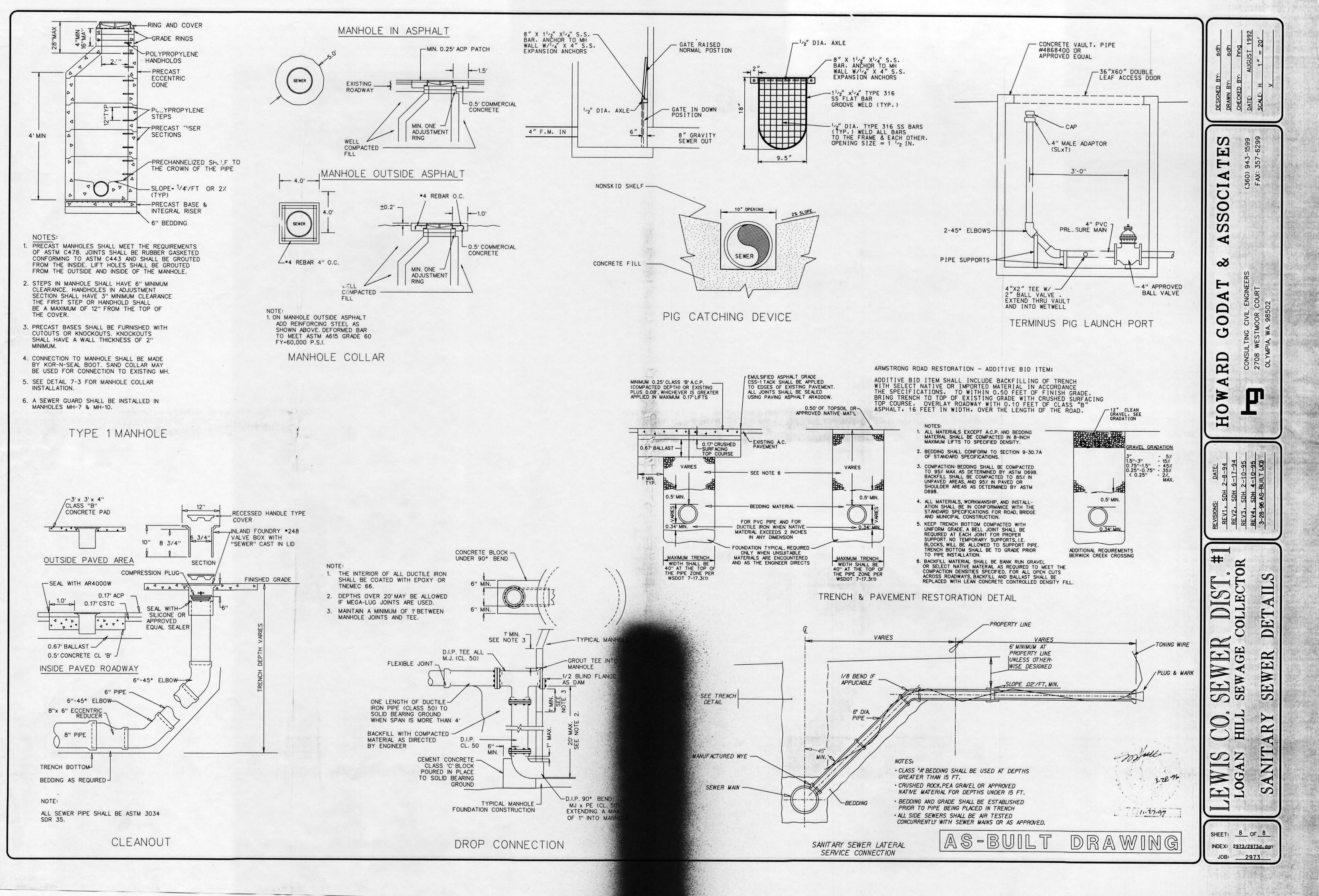
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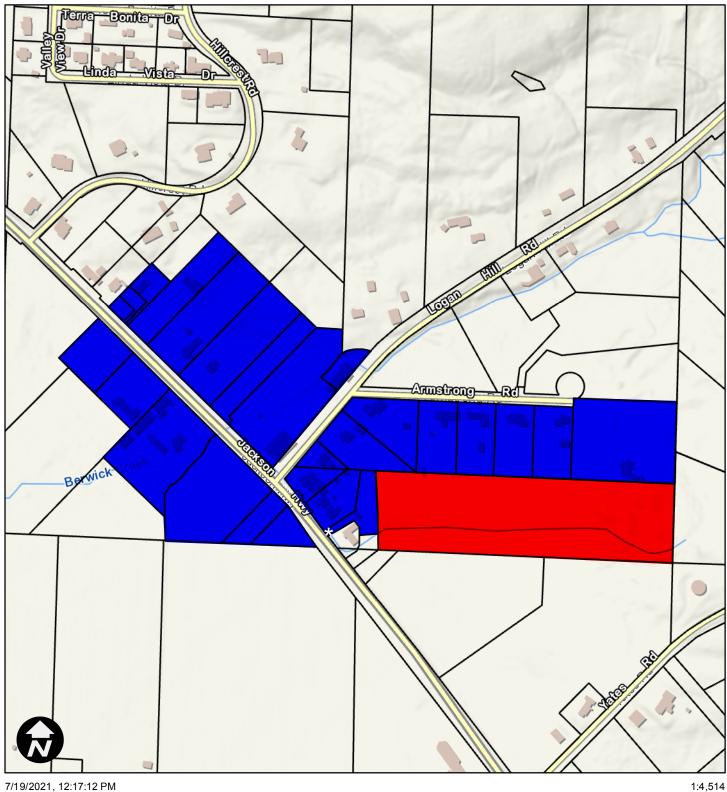
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Lewis County GIS Web Map





- **Proposed Development Location**
- Parcels Contributing to Lift Station
- Lift Station Location *

205 410 820 ft ٥ NAD 1983 StatePlane Washington South FIPS 4602 Feet

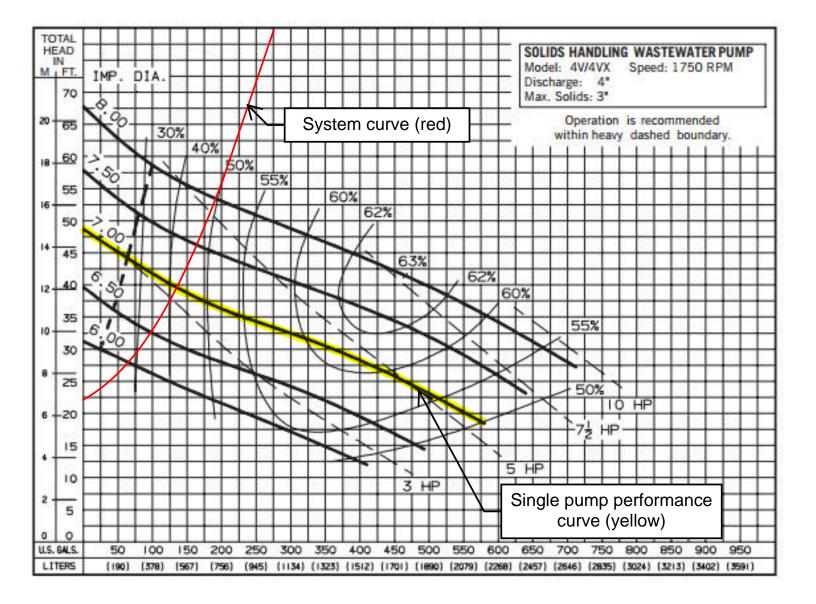




Lewis County does not guarantee the accuracy of the information shown on this map and is not responsible for any use or lease by others regarding this material. It is provided for general informational purposes only. This map does not meet legal, engineering, or survey standards. Please practice due diligence and consult with licensed experts before making decisions.

Pump Performance and System Curve:

Myers 4VX50M4-23 Hazardous 4" Solids Handling Wastewater Pump 5.0 HP 230V - yellow System Curve (calculated) - red



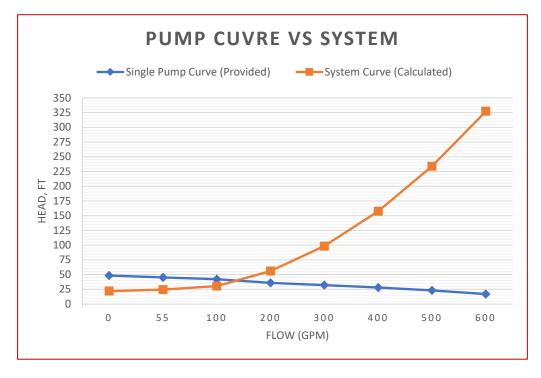
System Curve Equation:

$$h_p = \left\{ (z_1 - z_2) + \left[f\left(\frac{L}{D}\right) \left(\frac{Q^2}{2gA^2}\right) \right] \right\}$$

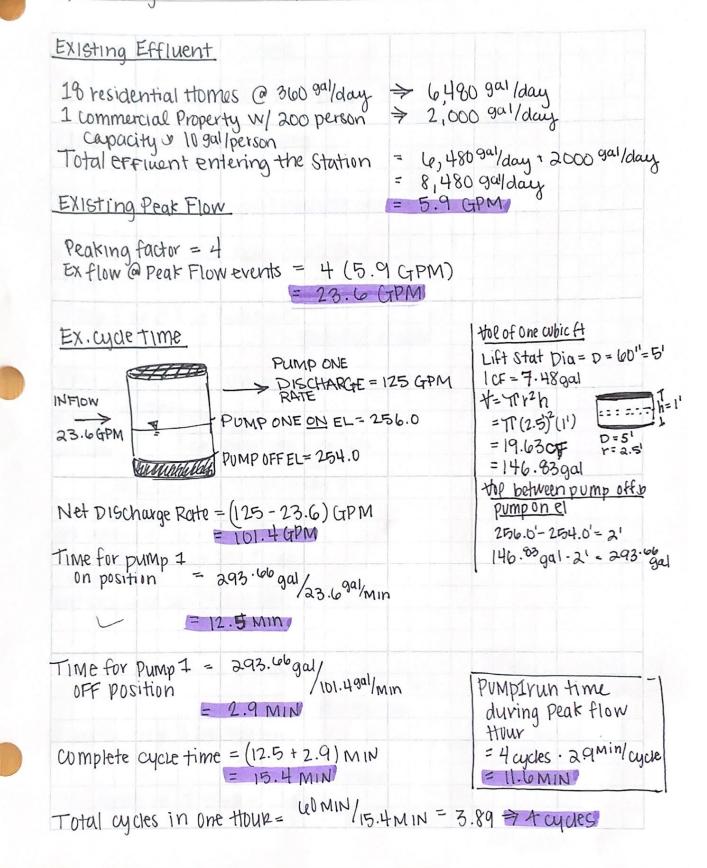
Where:

Highest Point in system, Z ₁	276
Pump Off, Z 2	254
Darcy Friction Factor, f	0.2
Pipe Length, L	1152
Inner Pipe Diameter, D	0.29
Pipe Cross Sectional Area, A	0.267

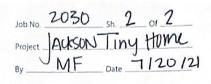
Flow (GPM)	Flow (CFS)	Single Pump Curve (Provided)	System Curve (Calculated)
0	0.00	48.5	22.00
55	0.12	45	24.57
100	0.22	42	30.48
200	0.44	36	55.92
300	0.67	32	98.33
400	0.89	28	157.69
500	1.11	23	234.02
600	1.33	17	327.31
667	1.48		399.30











subject Proposed conditions & cycle time

